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# **Mathematical Modelling of the Voltage Required for Separation of Cell-like Particles**

# **Ruchi Agarwala,\* and Beena Sandeep Limkar<sup>a</sup>**

<sup>a</sup>Department of Technology, Savitribai Phule Pune University, Pune, India

\*Corresponding author: ruchi.394ag@gmail.com

#### **ABSTRACT**

Microfluidic devices separate the cells by using dielectrophoresis, magnetic, acoustic, or other techniques. This study focuses on a voltage required in a microfluidic device that uses dielectrophoretic force to separate the cell-like particles based on their size difference. Numerical simulation shows that the particles separate above a certain minimum voltage and do not separate above a certain maximum voltage, which defines the particle separation range. This voltage requirement depends on cell and buffer solution parameters. This study uses data-sets generated using numerical simulation by varying these parameters. Detailed analysis of these data-sets gave the significant parameters, which decide the voltage requirement, as the size of the two cell-like particles and viscosity of the buffer solution. A mathematical model is developed using regression analysis, to calculate the voltage requirement, considering particle size ranging between  $2\mu$ m to  $30\mu$ m and viscosity ranging from 0.8cp to 4cp. The voltage predicted from the mathematical model is compared with the values obtained from the numerical simulation. The RMS error obtained for the entire data-set is 1.4412%. The mathematical model thus predicts the required voltage with good accuracy and will be helpful in healthcare, which needs frequent screening or testing of samples for early diagnosis of HIV, cancer, malaria, and many such applications.

**Keywords:** Dielectrophoresis, Electric voltage, Mathematical modeling, Microfluidics, Separation.

# **1. INTRODUCTION**

In today's world, the main concern of the researcher is to diagnose the disease for better health care. The clinical research is done by liquid biopsy, i.e. blood test which requires various complicated instruments with the large volume of blood as compared to micro and nanoliters [1]. There are many places where lab facilities are absent or it may be difficult to set up a proper lab, thus one can have a microfluidics platform for blood fractionation and sample preparation to perform the liquid biopsy. The main advantage of using these Lab-on-Chip phenomena for cell trapping and plasma analysis is that low blood volume is required. Results can be obtained in short duration because of its high integration, miniaturization and automation which helps it to diagnose the disease at an early stage [2, 3].

Various research activities have been carried out in the field of cell separation based on their cell dimensions and properties such as the magnetic properties of cells, adhesive properties, dielectric properties, etc. The cells can be separated by using two techniques i.e. by active technique or by passive technique. In active technique, the external field is used which include electric forces, acoustic forces, magnetic forces and mechanical forces, whereas the passive technique includes inertia forces, sorting due to adhesion, pinched flow, filtration and many more [4]. This study focuses on the voltage required in the separation of cells by using dielectric properties of the cells. It can be done with the help of dielectrophoresis as this force allows moving and separating the polarized particle in the non-uniform electric field. Dielectrophoresis (DEP) is derived from the electrophoresis technique in which there is no need to charge the particles [5]. It can move the particles in the DC or AC electric field by polarizing it in the non-uniform electric field without changing their biological properties and which does not damage the cells. In previous research, the dielectrophoresis has successfully been used for separating cancerous cells, infected blood cells and other blood components such as erythrocyte and leukocytes for diagnosing various illnesses [6, 7].

Pommer et al [8] have used a two-stage device for the separation of platelets from diluted whole blood in a microfluidic channel by using dielectrophoresis. The cell sorting has been performed based on the cell sizes. Park [9] has designed a device based on electrokinetics and electric field for the separation of pathogenic bacterial cells from the whole blood cells by using continuous dielectrophoresis. Piacentini [10] has used the microfluidic device for the separation of platelets from red blood cells and white blood cells by using dielectrophoresis field flow fractionation and hydrodynamic focusing by using a low applied voltage. Ali [11] has developed the numerical model for the

separation of red blood cells, white blood cells and platelets with the application of low voltage. It was used to count the number of cells separated and it also gave the different outlet design for efficient blood separation.

A. Dabighi [12] has made a microfluidic device used for separating tumor cells based on their physical properties by using dielectrophoresis force. R. Derkhshan [13] has used the approach of the DEP force to separate the three polystyrene particles with minimum electric potential. Y. Zhang [14] have used dielectrophoresis microfluidic chips for the separation of WBCs, RBCs and platelets.

The objective of this mathematical modelling is to generate the equation to calculate the voltage required to separate the particles ranging between 2µm to 30µm. This study uses the properties of dielectrophoresis field flow fractionation for the study of the different electrical and physical properties of the cells.

# **2. THEORETICAL BACKGROUND**

This section explains the theory related to the cells, electrical properties of the cells and their separation techniques from which dielectrophoresis is used in this study.

#### **2.1 Theory of cell**

The cells have different electrical properties such as its permittivity, conductivity, etc. All these electrical properties arise from the physical properties of the membrane and the ion channels in the membrane [10]. The cell membrane consists of a bilayer which acts as a dielectric medium between the salt solution and the cytoplasm, therefore the cell membrane acts as a capacitor. The membrane thickness ranges approximately between 7 to 10nm [15] and the healthy cells range between 2 to 15  $\mu$ m.

#### **2.2 Theory of Dielectrophoresis**

The field of dielectrophoresis was first studied by Herbert Pohe in the 1950s whereas it was published in 1978 [16]. Dielectrophoresis is a force which is used to move and thus separate the polarized particles or cells in the nonuniform electric field. As the advancement in the field of microfabrication and the lab on chip phenomenon have led to the development of dielectrophoresis [17]. The dielectrophoretic force arises when the polarized particle is placed in a non-uniform electric field and it is given by equation (1) [17]:

$$
F_{DEP} = 2\pi\varepsilon_o \varepsilon_m r^3 \text{Re}[K(\omega)] \nabla(E)^2
$$
 (1)

The factor Re  $[k(\omega)]$  depends on the frequency and the complex permittivity of the particle and the medium as it is given by equation (2):

$$
K(\omega) = \frac{\varepsilon_p^* - \varepsilon_m^*}{\varepsilon_p^* + 2\varepsilon_m^*}
$$
 (2)

Depending upon these properties, this factor can be positive or negative which gives rise to two types of dielectrophoresis i.e. if  $Re[K(\omega)]$  is negative then it gives rise to negative dielectrophoresis (nDEP) and when  $Re[K(\omega)]$  is positive then it is positive dielectrophoresis (pDEP). Positive DEP occurs when the

particle is more polarized than the medium in which it is surrounded i.e.  $\mathcal{E}_p \gg$ 

 $\varepsilon_m$  hence the particle will get attracted towards the area having high electric field whereas negative DEP occurs when the particle is less polarized than the

medium in which they are surrounded i.e.  $\mathcal{E}_p \ll \mathcal{E}_m$ .

Hence, the particle will move towards a low electric field. Positive DEP is effective for the medium having low conductivities therefore, the medium with high conductivities of  $>1$ S/m are suitable for negative DEP. Thus, in this study, we will be using negative DEP whose medium permittivity is much more than the permittivity of the particle. The field flow fractionation method has been used for the separation of the particle as it uses a low voltage to generate negative DEP force. It is a technique in which the force is applied perpendicular to the direction of flow to separate the particle which is present in the medium.

#### **3. NUMERICAL SIMULATION AND PARAMETER STUDY**

In this section, we have discussed the numerical simulation of the model and the number of parameters. These are used in the separation of two particles which are referred to as the diameter of one particle  $(D_1)$  and diameter of another particle  $(D_2)$ . Thus, a mathematical model is proposed which is used to separate the particles with an application of low voltage. This paper aims to model an equation of voltage required for the separation of particles of particular sizes which is done by using DEP forces as they are directly proportional to the size of the particles. Hence, particles can be separated by the same force with the variation in the voltage.

#### **3.1 Numerical Simulation**

In this paper, the 2D geometrical model of the microfluidic device is used for the separation of particles based on their size with the use of dielectrophoretic field-flow fractionation. This study uses the experimental model described by Piacentini and Renaud [10] which is used for the separation of two particles. The left side of the geometry has two inlet sections, from the upper inlet the blood is injected whereas from the lower inlet the buffer solution (PBS) is injected. The length of both the channels is 200 um and the width of the channel is 40µm. The electric voltages are applied in the separation region. All the electrodes have voltages of the same magnitude but with opposite polarity. The length of the electrode array of the geometry is 520µm as shown in Fig. 1. The right side of the geometry has the outlet section which has two outlet channels for the collection of two different particles whose lengths are 200µm and the angle between them is 90deg. Thus, the total length of the channel is approximately equal to 802.8427µm.

As per the study for the separation of cells, the simulation is performed in the COMSOL Multiphysics software as shown in Fig. 2 for the decided geometry. The values of the parameters used in the simulation are given in Table 1.



**Fig. 1.** Geometry of Micro-channel



**Fig. 2.** Model for Numerical Simulation

Sr. No.	<b>Parameters</b>	<b>Value</b>	Unit
1	<b>Fluid Conductivity</b>	1	S/m
2	<b>Fluid Permittivity</b>	80	
3	<b>Fluid Density</b>	1080	kg/m <sup>3</sup>
4	Fluid Dynamic Viscosity	1	cP
5	Particle Density of RBCs and Platelets	1050	kg/m <sup>3</sup>
6	Range of diameter $D_1$ and $D_2$	$2 - 30$	μm
7	Conductivity of particle	0.25	S/m
8	Permittivity of particle shell	6	
9	Relative Permittivity of particle	100	
10	Conductivity of particle shell	$1e-6$	S/m
11	Range of particle shell thickness	$6-10$	nm
12	Frequency	100	kHz

**Table 1.** Parameter values for numerical simulation

Various simulations are performed for the same set of values used in Table 2 by varying the magnitude of the voltages applied in the separation region. Thus, by varying the voltages it was observed that for the separation of two given particles there is the lowest voltage below which they will not separate as shown in Fig. 3. Further by increasing the voltage, it was observed that there is the highest voltage above which particle will not separate as shown in Fig. 4.

In Fig. 3 it is seen that the particles in the lower channel touch the left side of the wall. Hence, if we apply lower voltage the particles will move in the upper channel and do not separate. Therefore, it can be said that this is the minimum voltage which is required for the separation of two given cell-like particles, below which both the particles will move in the upper channel. Similarly, in Fig.4 it is observed that the particles in the upper channel touch the right side of the wall. Hence, if we apply higher voltage the particle will move in the lower channel and do not separate. Therefore, it can be said that this is the maximum voltage which is required for the separation of two cell-like particles, beyond which both the particles will move in the lower channel. Hence, it is clear that there is a range from the lowest voltage (LV) to the highest voltage (HV) for the same size of particle separation.

Sr. No.	Solution	<b>Dynamic Viscosity</b>
	Water	1cP
	<b>Blood</b>	3-4 cP [19]
	PBS Buffer	1 $\pm 0.05$ cP [20]
	Other Buffer	$0.8 - 1.5$ cP

**Table 2.** Dynamic Viscosity of different solutions



**Fig. 3.** Lowest voltage for the separation of particles



**Fig. 4.** Highest voltage for the separation of particles

#### **3.2 Parameters Study**

This section consists of the study of different parameters which are significantly used in the separation of particles. The parameters are classified as the buffer parameters, cell parameters and the parameters of the cell membrane. The study of a given parameter is done by keeping all other parameters constant for the given two particle size. Thus, in this section, these parameters are plotted against the lowest and the highest voltages required in the separation as discussed in section 3.1.

#### **3.2.1 Buffer parameters**

These are classified into three different parameters, i.e. fluid conductivity, fluid density and fluid viscosity. The variation of each parameter is studied against the lowest and the highest voltages by keeping the rest values to be constant. Thus the following graphs are obtained as shown in Fig. 5. In Fig. 5a, it is observed that the voltage decreases with the increase in the conductivity and

becomes constant after 500mS/m. The conductivity of the buffer solution ranges approximately between 1500 to 2000mS/m [18]. Thus, from the graph, it is clear that the conductivity remains constant for the given range. Therefore, conductivity does not contribute to the separation of particles. In Fig. 5b, it is observed that there is no change in the voltage with the increases in the fluid density which ranges between 1000 to 1100 kg/m<sup>3</sup> [18]. Thus, it does not affect the separation of particles. Fig. 5c shows the variation of viscosity with the voltage. It is observed that with the increase in the viscosity the voltage shows the power trend as shown in the equation (3). From the literature, it is studied that the range of dynamic viscosity for different solutions varies as given in Table 2. In this study, the range of viscosity from 0.8cp to 4cp is considered.

$$
V \propto \mu^{1/2}
$$
\n(a) Fluid Conductivity vs Voltage\n
$$
D_1 = \theta \mu m \rightarrow LV
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D_2 = 10 \mu m \rightarrow HV
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B = 10 \mu m \rightarrow HV
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B = 10 \mu m \rightarrow HV
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B = 10 \mu m \rightarrow RV
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B = 10 \mu m \rightarrow 100
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B = 10 \mu m \rightarrow 100
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B = 10 \mu m \rightarrow 100
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B = 10 \mu m \rightarrow 100
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D_1 = \theta \mu m \rightarrow -LV
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0 1 2 3 4 Dynamic Viscosity (cP)

0.0 0.5 1.0 1.5

Voltage

74

#### **3.2.2 Parameters of cell membrane**

These are again classified into three different parameters, i.e. shell conductivity, shell permittivity and shell thickness which are plotted against the lowest and the highest voltage as shown in the Fig. 6. In Fig. 6a, it is observed that the slope of the line is almost negligible. Thus, it can be treated as a constant voltage with the increase in the conductivity of the shell and that does not affect the separation of particles. In Fig. 6b, it is observed that the slope is almost equal to zero along the permittivity and in Fig. 6c, the voltage remains constant along the shell thickness therefore it does not play any role in the separation of particles.



**Fig. 6.** Parameters of cell membrane vs voltage

## **3.2.3 Particle properties**

This consist study of three different parameters, i.e. particle conductivity, particle density and particle permittivity which are plotted against the highest and the lowest voltage as shown in Fig. 7.



**Fig. 7.** Particle Properties vs Voltage

In Fig. 7a, 7b, 7c, it is observed that the variation between the particle density, conductivity and permittivity versus the applied voltage is observed to be constant. Hence, it does not contribute to the separation of the particles.

## **3.2.4 Particle dimensions**

This gives the variation between the size of the particles with the applied voltages by keeping all other parameters constant.



**Fig. 8.** Particle Dimensions vs Voltage

Thus, the graph obtained for different dimensions is shown in Fig. 8. In Fig. 8a, it is observed that the highest voltage varies with the increase in the diameter  $D_1$ whereas the lowest voltage remains constant with an increase in  $D_1$  by keeping  $D_2$  constant. In Fig. 8b, it is observed that the lowest voltage varies with the increase in the diameter  $D_2$  whereas the highest voltage remains constant with the increase in  $D_2$  by keeping  $D_1$  constant.

## **4. MATHEMATICAL MODELING AND VALIDATION**

In this section, the mathematical equation is modelled for the electric voltage required in the separation of given two particles. From section 3.2 it is clear that the voltage depends upon the two main parameters which are particle dimensions and the fluid viscosity. Thus, in the latter part of this section, these parameters are validated with the values obtained by the mathematical model and the results are plotted as shown.

#### **4.1.Mathematical Modeling**

In this section the mathematical equation is modelled for the voltage which depends on  $D_1$ ,  $D_2$  and the dynamic viscosity of the fluid. As explained in section 3.1 the given two particles are separated between the lowest and the highest voltage. Thus, the effect of the lowest and the highest voltage is studied with the increase in the size of the particle dimensions.

#### **4.1.1 Study of lowest voltage**

The study for the lowest voltage is classified into two parts i.e.  $D_2/D_1 > 1$  and  $D_2/D_1 < 1$  where the diameters are varied from 2 $\mu$ m to 30 $\mu$ m. Thus from the Fig. 9a it is observed that for the ratio of  $D_2/D_1 > 1$  the lowest voltage remains constant with the increase in the size of  $D_1$ . Whereas from the Fig. 9b it is observed that the lowest voltage decreases as  $D_2$  increases from 2 $\mu$ m to 30 $\mu$ m. Thus, it can be said that the lowest voltage is dependent only on  $D_2$  and  $D_1$  does

not contribute to the same. For the ratio  $D_2/D_1 < 1$  voltage decreases with the increase in  $D_1$  and remains constant along with  $D_2$  as shown in the Fig. 9c, 9d without the change in the coefficients.





**Fig. 9.** Particle size vs Lowest voltage

#### **4.1.2 Study of highest voltage**

This study is again classified into two parts i.e.  $D_2/D_1 > 1$  and  $D_2/D_1 < 1$ . It is observed from the simulation that within this ratio it is further divided into another two parts i.e. for the ratio of  $D_2/D_1 > 1$  it is divided as  $D_2/D_1 < 2.5$  and  $D_2/D_1 > 2.5$ . This is because it is observed that as  $D_2$  exceeds 2.5 times  $D_1$  it gets stuck to the lower wall of the separation region. Hence, the particle cannot move further in the channel as shown in Fig. 10.



**Fig. 10.** Highest voltage for ratio  $D_2/D_1 > 2.5$ 

Thus, to separate the particle it is needed to apply the lower voltage and due to it the trend of the line changes above this ratio. It is observed that the highest voltage for the ratio of  $D_2/D_1 < 2.5$  the separation depends on  $D_2$  and remains constant along  $D_1$  as shown in Fig. 11c and Fig. 11d. Similarly for the ratio  $D_2/D_1 < 1$  will be classified as  $D_1/D_2 < 2.5$  and  $D_1/D_2 > 2.5$ . For the ratio  $D_1/D_2$  $\leq$  2.5 the highest voltage remains constant along  $D_1$  and varies with the increase of  $D_2$ . Whereas for  $D_1/D_2 > 2.5$  the voltage depends on  $D_1$  and remains constant along with  $D_2$ .



**Fig. 11.** Particle size vs Highest voltage

From the simulation done in section 3.1 and Fig 3 and 4 shows that the highest and the lowest voltages applied for the separation of any given two particles are very close to the wall.

This may destroy or rupture the cell thus to avoid this situation the average of this voltage can be applied to separate the particle at the particular voltage. Thus, the average voltage is given by equation (4) and whose lowest and highest voltages are given in Table 3. Thus, by using equation (4) one can separate the two given particles between the range of 2µm to 30µm at a particular voltage.

$$
V = \left(\frac{V_L + V_H}{2}\right) \mu^{1/2} \tag{4}
$$

<b>Voltage</b>	$D_2/D_1 > 1$		$D_2/D_1 < 1$	
$V_{L}$	$a_1D_2^{-a_2}$		$a_1D_1^{-a_2}$	
	$D_2/D_1 \le 2.5$	$D_2/D_1 > 2.5$	$D_1/D_2 \le 2.5$	$D_1/D_2 > 2.5$
$V_H$	$b_1D_1^{-b_2}$	$c_1D_2^{-c_2}$	$b_1D_2^{-b_2}$	$c_1D_1^{-c_2}$
Where: $a_1 = 19.100$ ; $a_2 = 0.985$ ; $b_1 = 19.384$ ; $b_2 = 0.996$ ; $c_1 = 50.695$ ; $c_2 = 1.003$				

**Table 3.** Lowest and Highest Voltages

#### **4.2.Validation**

In this section, the results obtained from the numerical simulation are compared with the results obtained by the mathematical model in section 4.1. Hence, their root mean square error is calculated for these two results by considering a different range of particle dimensions and the dynamic viscosity of the fluid.

The Fig. 12 shows the validation of results between  $D_2$  versus required average voltage for different diameters of  $D_1$  with their root mean square (RMS) error which is given in table 4.

**Table 4.** Validation of results for particle dimensions

Fig.13		Size of D <sub>1</sub> ( $\mu$ m)   RMS error (%)   Fig.13   Size of D <sub>1</sub> ( $\mu$ m)   RMS error (%)	
a	2.6959		1.0656
	0.2879		0.3008



Fig. 12. D<sub>2</sub> vs Average voltage

The numerical and the analytical values for the fluid viscosity against the voltage are plotted in the Fig. 13 and it is observed that the root mean square error is equal to 0.1495%, which is approximately equal to the numerical values. The RMS error calculated for all the 1450 combinations of data-sets is found to be 1.4412%. Hence, it can be seen that the values calculated from the mathematical model are almost equal to the values obtained from the numerical data. Hence, the model prepared to calculate the voltages is approximately correct as it shows good accuracy**.** 



**Fig. 13.** Fluid viscosity vs Voltage

# **5. CONCLUSION**

Microfluidics is used for separation of cell-like particles required for diagnostic purposes. This study focuses to detect the voltage required for separating two cell-like particles. From the numerical simulation, it is observed that the particles separate above a certain voltage and on further increasing the voltage, it is observed that the particles do not separate above a certain voltage value. Thus, there exists the voltage range in which the particle separates. It is also observed that at the lowest and the highest voltage values the cell-like particles touch the wall of the channel which may damage the cell. Thus, it is recommended to apply an average voltage which will prevent the cell from sticking the channel walls. Hence, a mathematical model is prepared to calculate the average voltage required in the separation of two cell-like particles.

The parameters, such as the cell geometry, cell properties and buffer solution properties are studied in detail to study their contribution to the required voltage. It is observed that the size (diameter) of the two cell-like particles and the dynamic viscosity of the buffer solution are the significant parameters affecting the values of voltage required in the cell separation. Other properties such as density, permittivity and conductivity of cell particles and its membrane do not contribute to the voltage required for separation of the cell-like particles.

This model considers the particle size (diameter) ranging from 2µm to 30µm which include both healthy and unhealthy cells and the dynamic viscosity ranging between 0.8cp to 4cp.

Further, the results obtained from the numerical simulation are compared with the values of the voltages predicted from the formulated mathematical model. Whereas the RMS error for the entire data-set of size variation is observed to be 1.4412%. Thus, the model predicts the voltage required in the separation of two cell-like particles with good accuracy. It is recommended that the developed model can be used for finding voltage required using the channel geometry considered for this study.

# **NOMENCLATURE**



# **REFERENCES**

- 1. N. Demierre, T. Braschler, R. Muller and P. Renaud, Focusing and continuous separation of cells in a microfluidic device using lateral dielectrophoresis, Sensors and Actuators B: Chemical 132, 2008, 388– 396.
- 2. H. Mohamed, Use of microfluidic technology for cell separation, Blood Cell-An Overview of Studies in Hematology, 2012, 195–226.
- 3. L. Spigarelli, V. Bertana, D. Marchisio, L. Scaltrito, S. Ferrero, M. Cocuzza, S. Marasso, G. Canavese and C. Pirri, A passive two-way microfluidic device for low volume blood-plasma separation, Microelectronic Engineering 209, 2019, 28–34.
- 4. C. W. Shields IV, C. D. Reyes and G. P. L´opez, Microfluidic cell sorting: a review of the advances in the separation of cells from debulking to rare cell isolation, Lab on a Chip 15, 2015, 1230–1249.
- 5. C. Li, X.-L. ZHENG, H. Ning, Y. Jun, L. Hong-Yan, F. Jiang and L. Yan-Jian, Research progress on microfluidic chip of cell separation based on dielectrophoresis, Chinese Journal of Analytical Chemistry 43, 2015, 300–309.
- 6. Y. Shen, Y. Yalikun and Y. Tanaka, Recent advances in microfluidic cell sorting systems, Sensors and Actuators B: Chemical 282, 2019, 268–281.
- 7. N.-T. Nguyen, S. T. Wereley, and S. A. M. Shaegh, Fundamentals and applications of microfluidics. Artech house, 2019.
- 8. M. S. Pommer, Y. Zhang, N. Keerthi, D. Chen, J. A. Thomson, C. D. Meinhart and H. T. Soh, Dielectrophoretic separation of platelets from diluted whole blood in microfluidic channels, Electrophoresis 29, 2008, 1213–1218.
- 9. S. Park, Y. Zhang, T.-H. Wang and S. Yang, Continuous dielectrophoretic bacterial separation and concentration from physiological media of high conductivity, Lab on a Chip 11, 2011, 2893–2900.
- 10. N. Piacentini, G. Mernier, R. Tornay and P. Renaud, Separation of platelets from other blood cells in continuous-flow by dielectrophoresis field-flow-fractionation, Biomicrofluidics 5, 2011, 034122.
- 11. H. Ali and C. W. Park, Numerical study on the complete blood cell sorting using particle tracing and dielectrophoresis in a microfluidic device, Korea-Australia Rheology Journal 28, 2016, 327–339.
- 12. A. Dabighi and D. Toghraie, "A new microfluidic device for separating circulating tumor cells based on their physical properties by using electrophoresis and dielectrophoresis forces within an electrical field," Computer methods and programs in biomedicine, vol. 185, 2020, p. 105147.
- 13. R. Derakhshan, A. Ramiar, and A. Ghasemi, "Numerical investigation into continuous separation of particles and cells in a two-component fluid flow using dielectrophoresis," Journal of Molecular Liquids, 2020 p. 113211.
- 14. Y. Zhang and X. Chen, "Blood cells separation microfluidic chip based on dielectrophoretic force," Journal of the Brazilian Society of Mechanical Sciences and Engineering, vol. 42, pp. 1–11, 2020.
- 15. J. L. Hall, Cell membranes and ion transport, Technical report, 1977.
- 16. H. A. Pohl, Dielectrophoresis, The behavior of neutral matter in nonuniform electric fields .
- 17. D. Li, Encyclopedia of microfluidics and nanofluidics, Springer Science & Business Media, 2008.
- 18. F. Biosolve Chimie 20 Rue Roger Husson, 57260 Dieuze, Sterile pbs buffer, 10x concentrate, PBS Buffer 10X (sterile) Molecular biology .
- 19. R. E. Wells and E. W. Merrill, Influence of flow properties of blood upon viscosityhematocrit relationships, The Journal of clinical investigation 41, 1962, pp. 1591–1598.
- 20. Fluxion, Understanding effects of viscosity in the bioflux system.

#### **Cite this article**

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